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SAPPHIRE SHAPED CRYSTALS: FROM THZ-WAVE DELIVERY TO SUPER-RESOLUTION IMAGING

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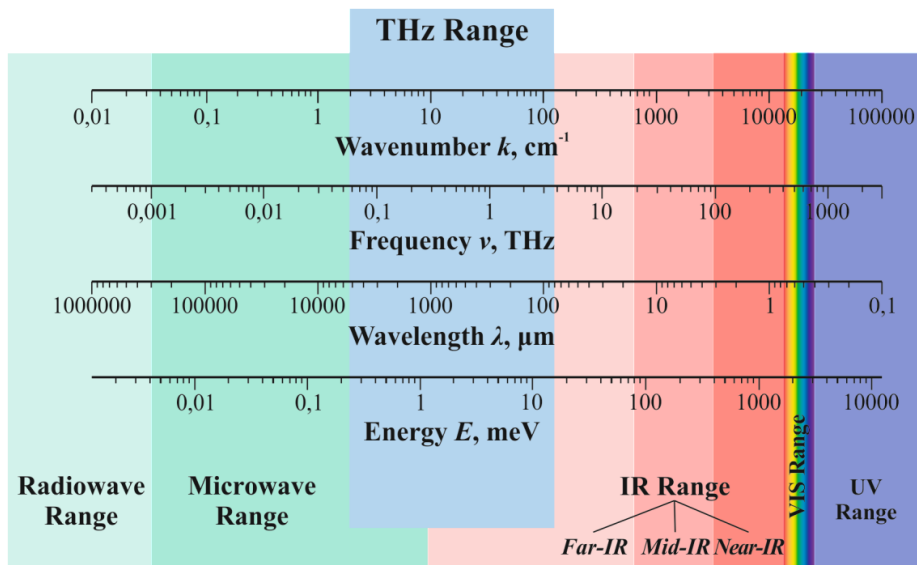
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OUTLINE OF THE TALK

- Optical elements designing for THz radiation delivery
 - Sapphire hollow-core waveguides for low-loss radiation delivery
- Attempts to improve the spatial resolution of THz imaging
 - Bundles of metal-coated sapphire fibers for THz sub-wavelength imaging
 - Tapered all-dielectric optical bundles for sub-wavelength imaging with using diffraction limited optics

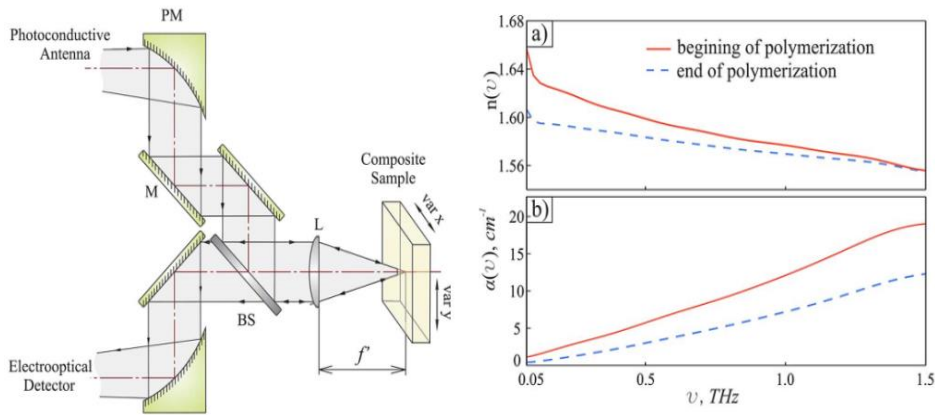
Optical elements designing for THz radiation delivery

THz radiation



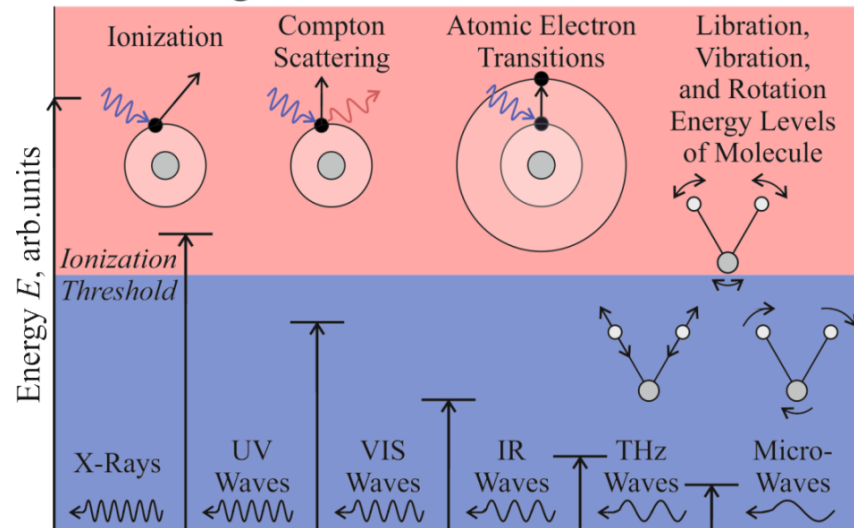
[H. Rubens & E. Nichols, "Heat rays of great wave length," *Physical Review (Series I)* **4**, 314 (1897)]

THz Pulsed Spectroscopy for Non-Destructive Evaluation of Polymers

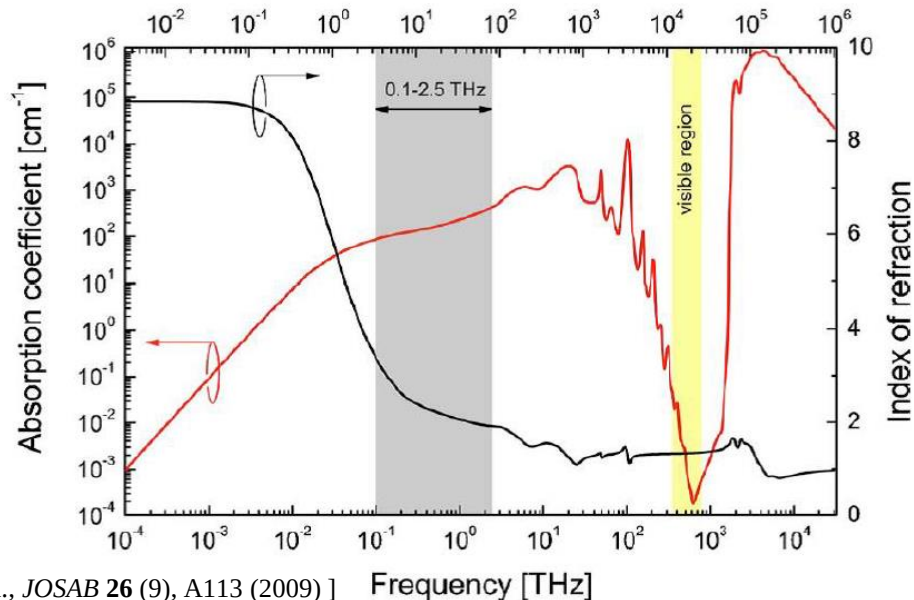


[K.I. Zaytsev et al, *IEEE Tr.Ter.Tech.*, 5(5), 810 (2015)]

Electromagnetic Radiation – Matter Interactions

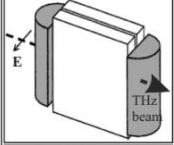
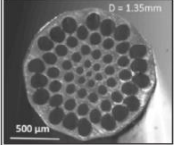
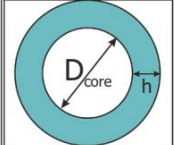
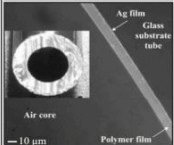
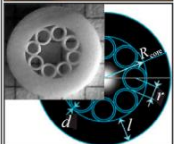
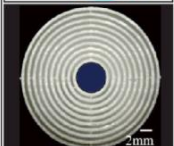


Wavelength λ , arb. units
Broadband dielectric response of water
 Wavenumber [cm⁻¹]



[U. Moller et al., *JOSAB* 26 (9), A113 (2009)]

THz Waveguiding Technologies

#	Waveguide	Cross-section	Spectral range, THz	Losses α , cm^{-1}	Material	Sizes	Comments
1	Parallel plate		0.1 - 4.0	$\alpha < 0.1$ near $\nu = 0.4, 1.4$ and 2.8 THz; $\alpha > 0.2$ near 4.0 THz	Copper	Separation plate $d=108 \mu\text{m}$ $L=24.4 \text{ mm}$	Guiding mechanism: reflection from metal
2	Graded step-index		0.2 - 1.5	increase from 0.025 to 0.15	Low density polyethylene (LDPE); $\alpha_{\text{mat}}=0.2 \text{ cm}^{-1}$, for $\nu=1.0 \text{ THz}$	5 rings of holes $D_{\text{out}}=1.35 \text{ mm}$ $L=20 \text{ cm}$	Guiding mechanism: total internal reflection (TIR); dispersion $< 1 \text{ ps/THz/cm}$; single mode below 0.35 THz
3	Porous Step-index		0.2 - 0.4	$0.035+3.1\nu^2$ [THz ²]	Silk foam; $n_{\text{mat}}=1.057$ $\alpha_{\text{mat}}=0.9$ for $\nu=0.3 \text{ THz}$	$D_{\text{out}}=5 \text{ mm}$ $L=20 \text{ cm}$	Guiding mechanism: TIR; dispersion $\approx 10 \text{ ps/THz/cm}$; 94% porosity of material
4	Hollow tube		0.3 - 1.0	decrease from 0.05 to 0.5	Polymethylmethacrylate (PMMA); $\alpha_{\text{mat}}=21.0 \text{ cm}^{-1}$, for $\nu=1.0 \text{ THz}$	$D_{\text{core}}=4 \text{ mm}$ $h=2.95 \text{ mm}$	Guiding mechanism: anti-resonant (ARROW); dispersion $< 10 \text{ ps/THz/cm}$; high absorbing cladding
5	Hollow tube with coating		2.5	0.0011 cm^{-1}	Hollow tube: silica glass, Cladding: polystyrene+Ag	$D_{\text{core}}=2.2 \text{ mm}$ $D_{\text{film}}=8.2 \mu\text{m}$ (Ag-film= $1 \mu\text{m}$)	Guiding mechanism: reflection/ARROW; CDP is used for PS-Ag deposit film
6	Two-wire plasmonic		0.03 - 0.5	increase from ~ 0.003 to 0.015	Wires: stainless steel, Cladding: Styrofoam	$D_{\text{wire}}=0.3 \text{ mm}$ $L=24 \text{ cm}$ wire separation: 0.5 cm	Guiding mechanism: plasmonic; demonstrated THz guiding through commercial TV-cable
7	Revolver multichannel		0.5 - 2.5	$\alpha_{\text{mat}}=0.017$ $\nu=2.1 \text{ THz}$	Polypropylene (PP); $\alpha_{\text{mat}}=0.2 \text{ cm}^{-1}$, for $\nu=1.0 \text{ THz}$	$d=0.06 \text{ mm}$ $r=0.4 \text{ mm}$ $D_{\text{core}}=1.3 \text{ mm}$ $D_{\text{outer}}=4.45 \text{ mm}$ $l=0.79 \text{ mm}$	Guiding mechanism: ARROW; dispersion $< 1 \text{ ps/THz/cm}$; 3 transparency band near 0.7, 1.4, and 2.1 THz
8	PC omniguide		0.1 - 0.3	$\alpha_{\text{mat}}=0.12$ $\nu=0.18 \text{ THz}$	Printing resin (PlasClear, Asiga); $\alpha_{\text{mat}} \approx 1 \text{ cm}^{-1}$, for $\nu=0.18 \text{ THz}$	$D_{\text{core}}=4.5 \text{ mm}$ resin layer - $512 \mu\text{m}$ air layer - $512 \mu\text{m}$ $N_{\text{bilayer}}=10$	Guiding mechanism: Photonic Bandgap (PBG); have been used as a biosensor with sensitivity $\approx 0.1 \text{ GHz}/\mu\text{m}$

Mean features of **polymer** materials in THz:

- relatively low radiation losses;
- high manufacturability (it is possible to produce the waveguides with complex cross—sections);
- relatively low refractive index;
- high sensitivity to the outer environment (for the most polymers);
- high dispersion in many cases.

Mean features of **crystalline** materials in THz:

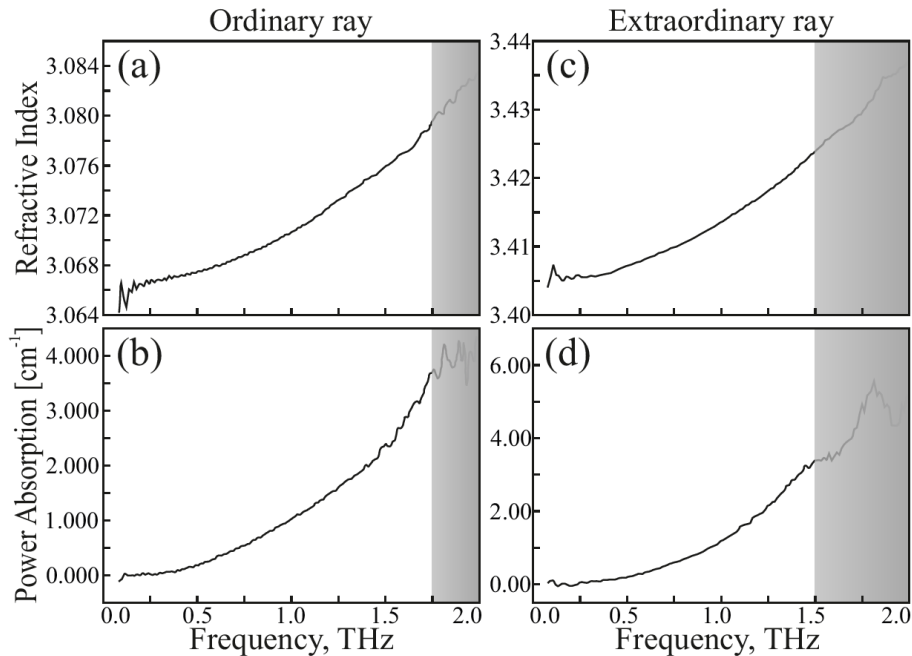
- low radiation losses and high refractive index;
- High resistivity (thermal, chemical, etc.)
- High hardness of material prevent to produce waveguides with complex shape

Moreover, all this types of THz waveguides can not be used for THz measurements in aggressive environments, in high temperature/pressure, in particular!

For example, they can damaged from medical sterilization

Shaped Sapphire – Key to THz delivery via hollow-core waveguides

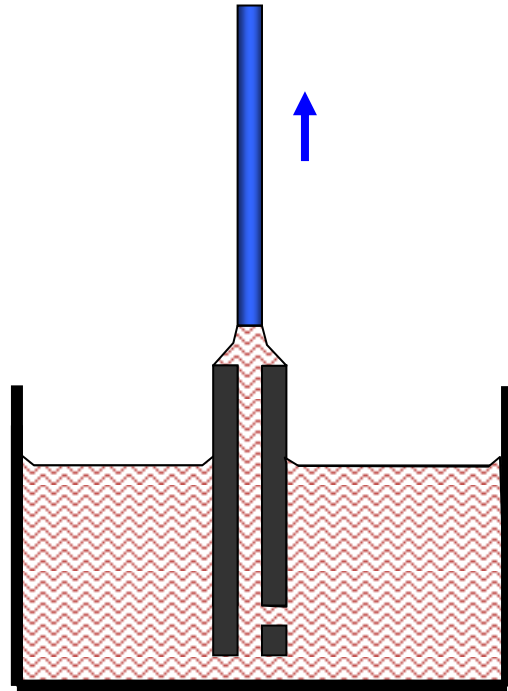
Refractive index (a, c) and extinction coefficient (b, d) of sapphire



Transparency and radiation strength	
Electromagnetic transparency (or translucency)	$0.2 \mu\text{m} < \lambda < 5 \mu\text{m}$ $\lambda > 200 \mu\text{m}$
Electromagnetic wave strength	Sustain high-power beams in VIS & IR spectral ranges
Radiation strength	No changes in IR transmission and VIS coloration after exposure to $10^7 - 10^8 \text{ Rad}$ for 60 min at -195°C
Thermal properties	
Melting point	2053°C
Maximum use temperature	1800°C
Thermal conductivity	$41.9 \text{ W/(m}\cdot\text{K)}$
Thermal coefficient of expansion	$5 \times 10^{-6} - 5 \times 10^{-6} \text{ K}^{-1}$ at 323 K

- High melting point (higher than 2000 K)
- Broad transmission band spanning the UV, visible, and IR bands
- High tensile strength
- High chemical and thermal shock resistance
- Biocompatibility
- High hardness (9 degree on Mohs scale)
- High specific heat
- Low friction coefficient ($(3.24-5.66)10^6 \text{ K}^{-1}$)

Shaped crystal growth techniques



Edge-defined film-fed growth (EFG),

on the basis of the
Stepanov concept

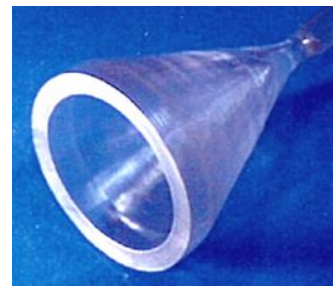
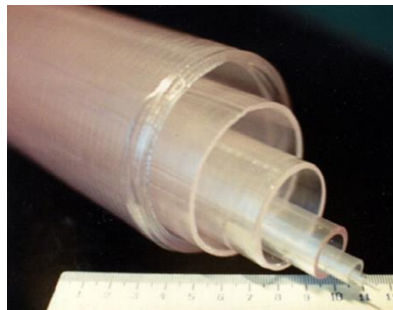
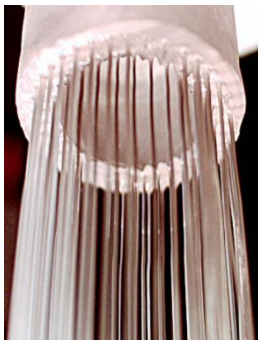
cross-sections of shaped crystals are very close to the final geometry

minimizing volume of labor efforts and corresponding losses of materials

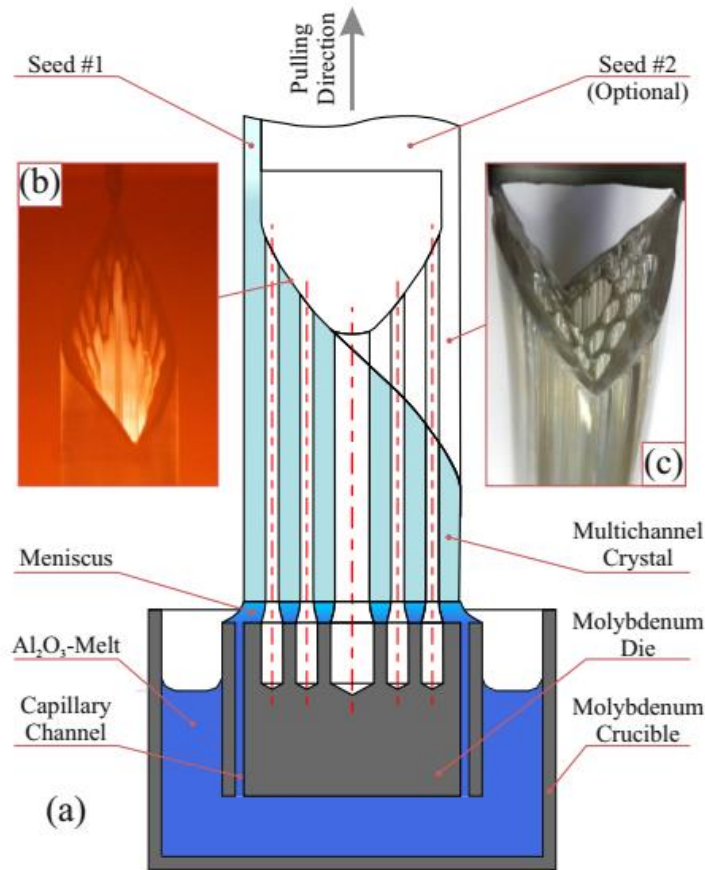
growth of crystals with shapes which impossible to grow or prepare from bulk crystals

high growth rates

new fields of applications

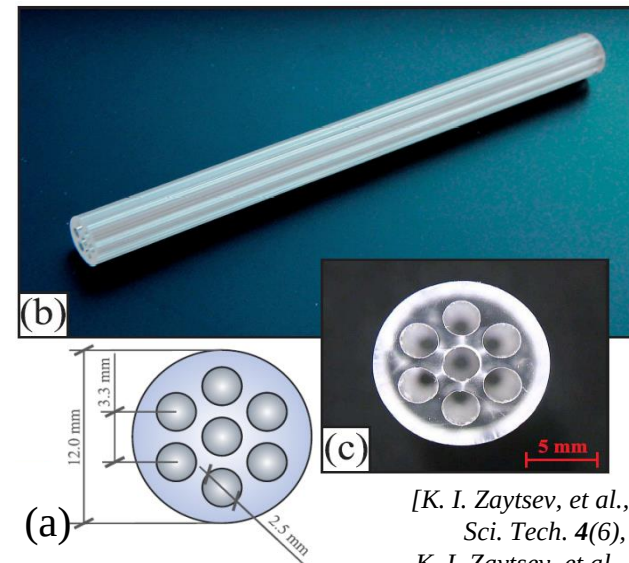


THz Waveguide Manufacturing Based on Shaped Sapphire Crystal



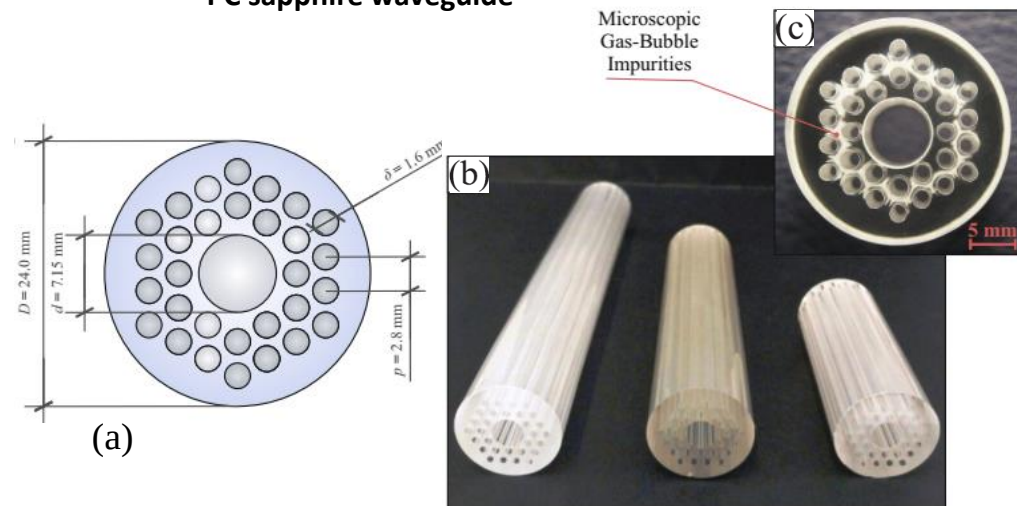
[V. N. Kurlov and S. N. Rossolenko, *J. Cryst. Growth* **173**(3–4), 417–426 (1997);
P. I. Antonov and V. N. Kurlov, *Cryst. Reports* **47**(1), S43–S52 (2002);
G.M. Katyba, et al., *Proc. of SPIE*, 103331C (2017);
Katyba, G.M. et al., *Progress in Crystal Growth and Characterization of Materials* (2018)].

ARROW sapphire waveguide

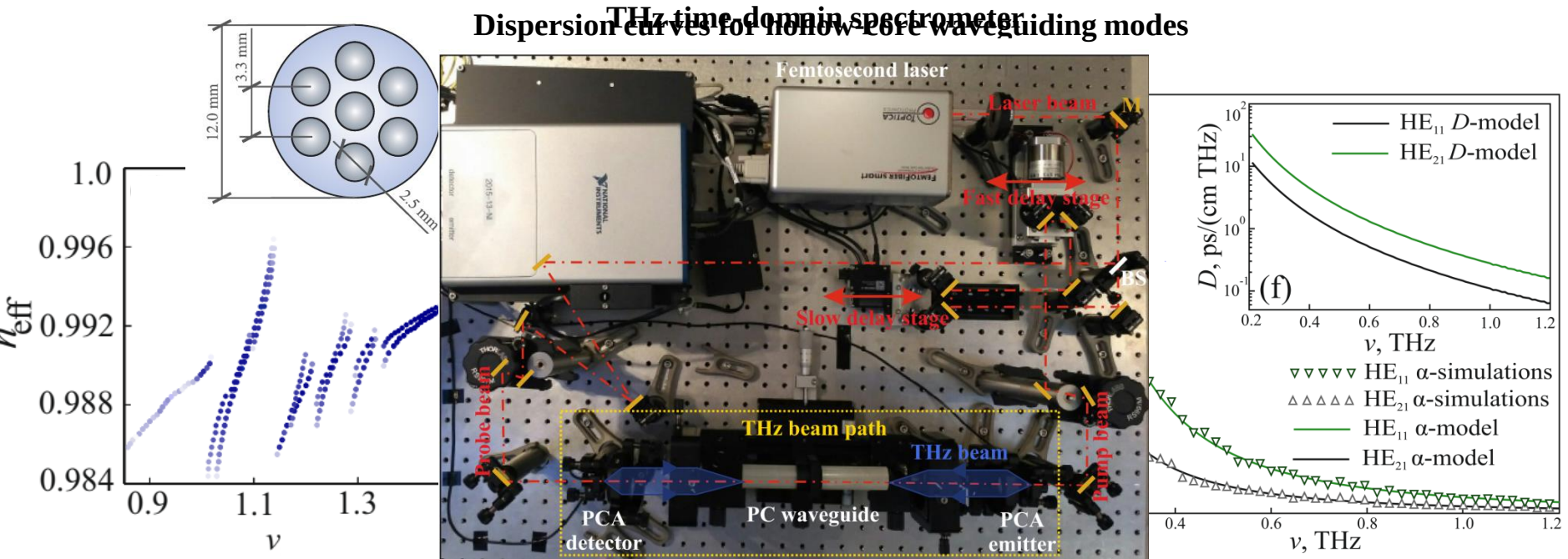


[K. I. Zaytsev, et al., *IEEE Trans. Ter. Sci. Tech.* **4**(6), 576, (2016);
K. I. Zaytsev, et al., *J. Phys. Conf. Ser.*, **673**(1), 012001 (2016)].

PC sapphire waveguide

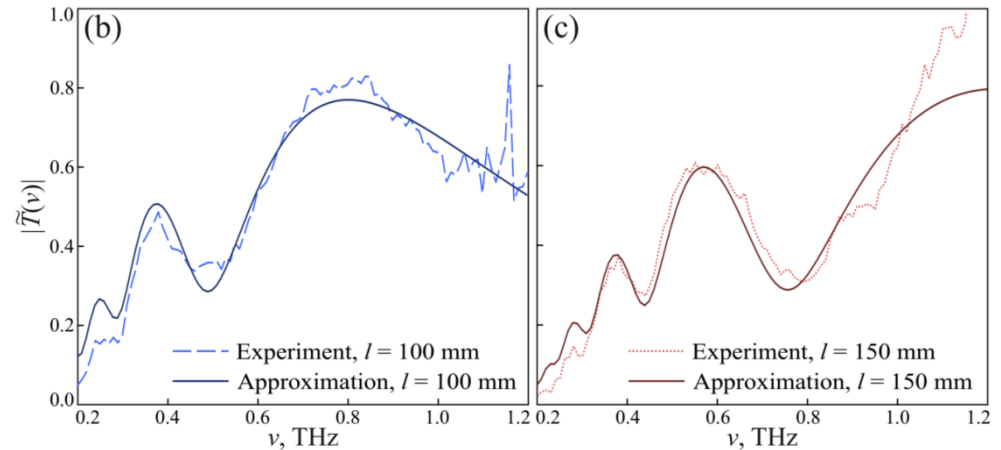
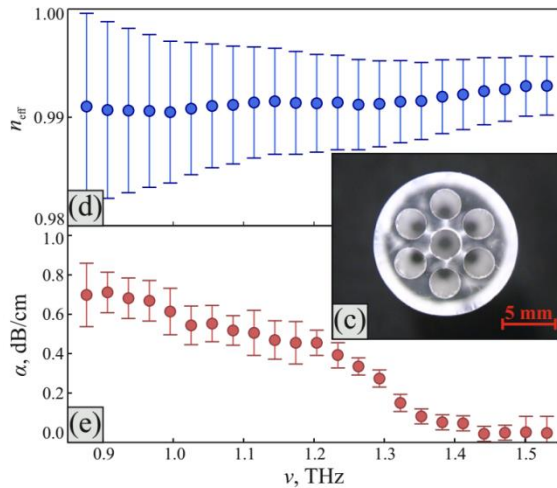


THz Waveguiding in Shaped Sapphire: Numerical Analysis and Experimental Results



[G.M. Katyba, et al., Adv.Opt.Mat.,(2018); K. I. Zaytsev, et al., IEEE Trans. Ter. Sci. Tech. 4(6), 576, (2016)].

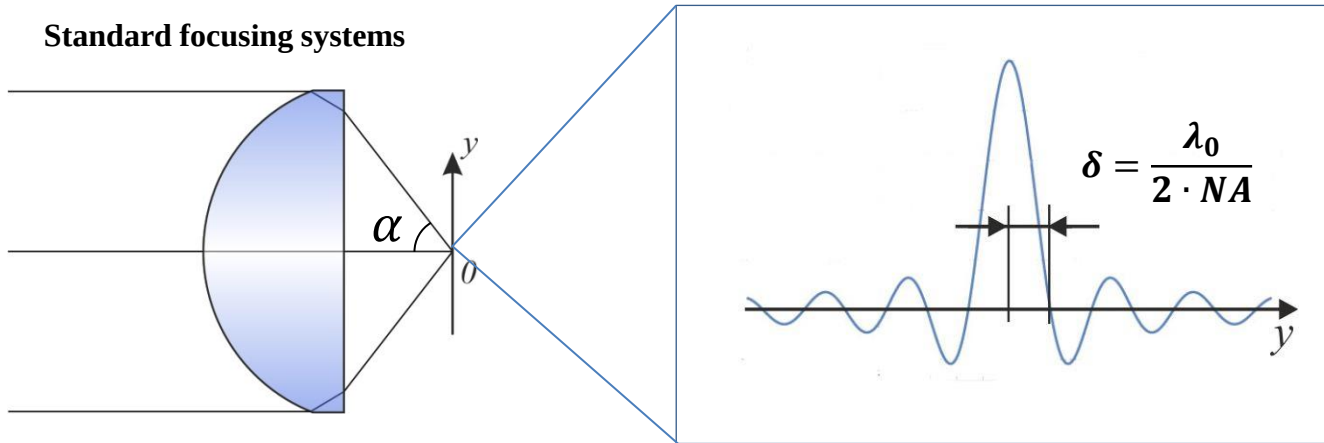
A model-based approximation of the experimental THz PC waveguide transmission



Attempts to improve the spatial resolution of THz imaging

INCREASING OF SPATIAL RESOLUTION OF THZ SENSING AND VISUALIZATION

Problem of low spatial resolution of THz spectroscopy and imaging



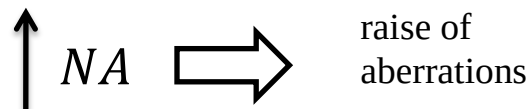
Spatial resolution (SP) is limited by electromagnetic wavelength ($\lambda \cong 300 \mu m$ or 1 THz) and numerical aperture $NA = n \cdot \sin \alpha$

$$\max\{NA\} = n$$

$$\delta = \frac{\lambda_0}{2 \cdot n} \quad \text{Abbe diffraction limit}$$

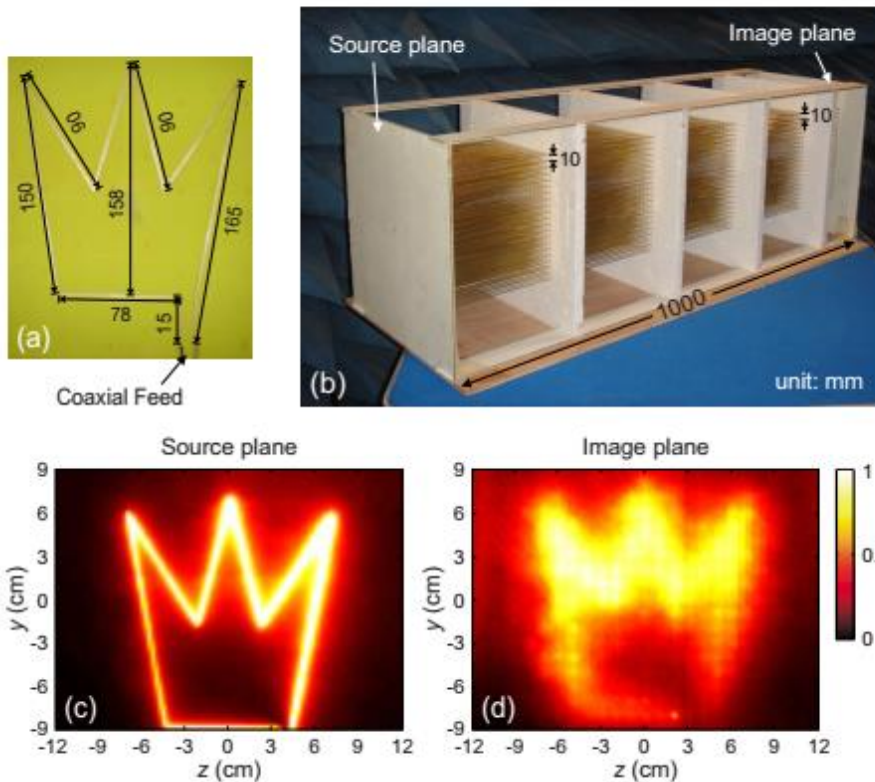
$$\text{For } n=1 \text{ (air)} \quad \delta = \frac{\lambda_0}{2}$$

It is necessary to increase the NA to achieve high SP



THz IMAGING USING THE FIBER BUNDLES

Example: microwave fiber endoscope

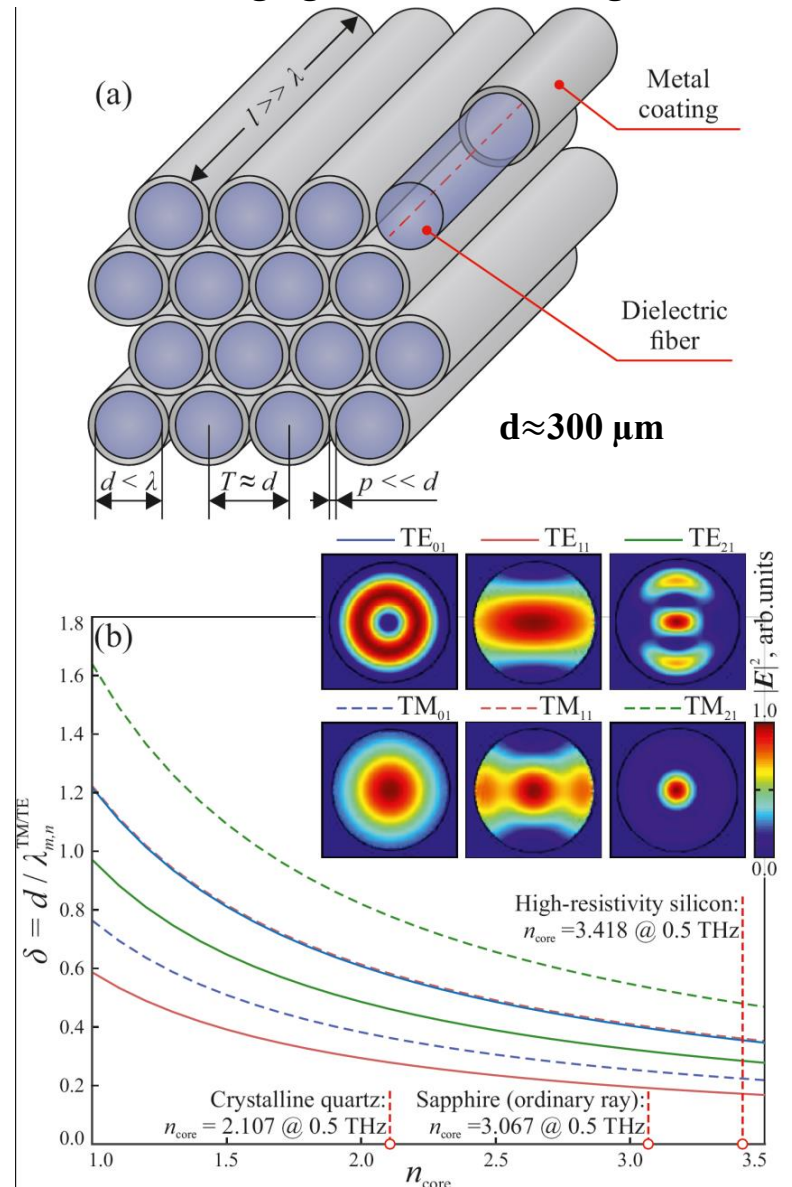


Minimal resolution– $\lambda/200$

[Belov P. A., et al. Appl. Phys. Lett. 97, 191905 (2010)]

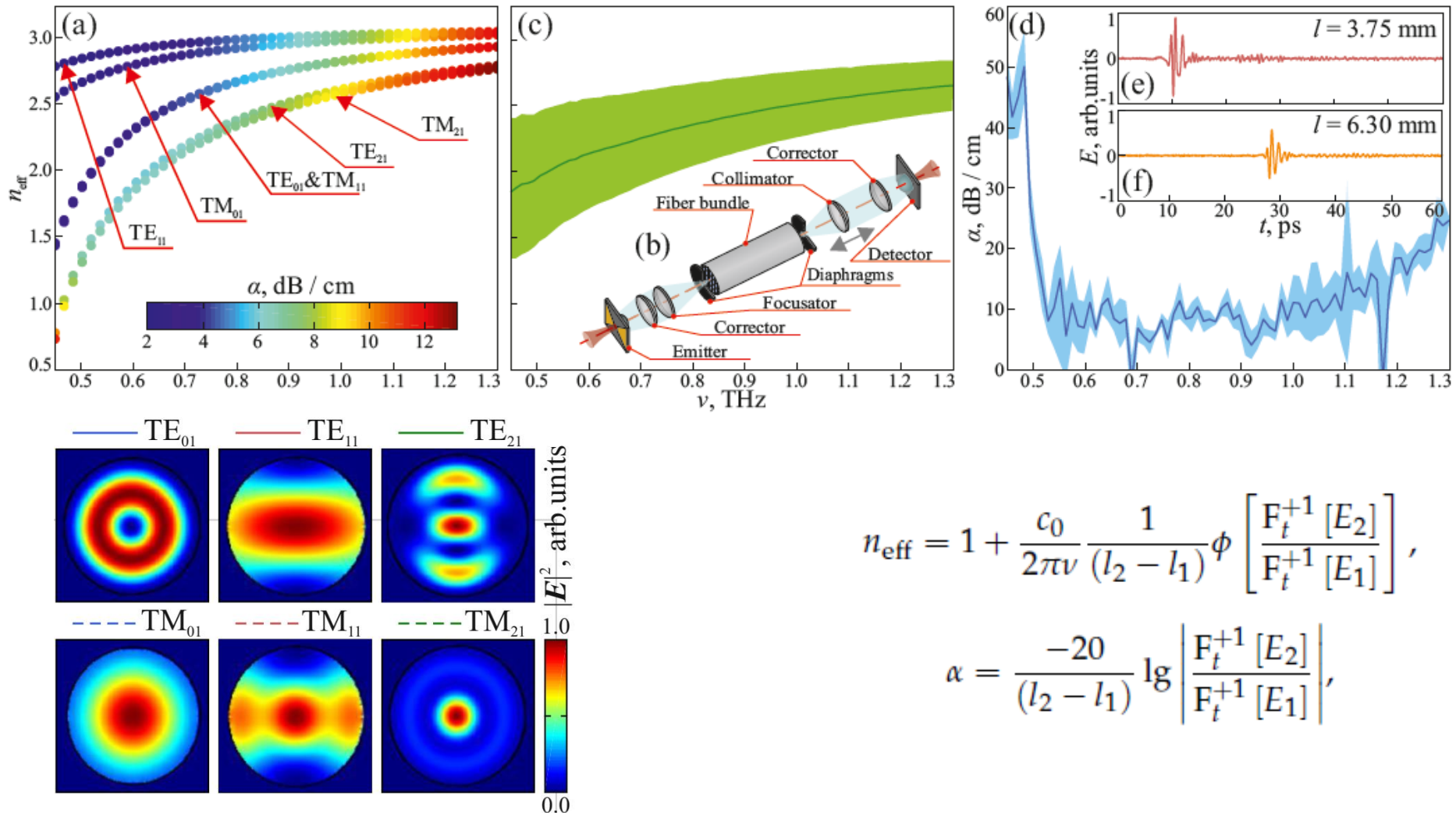
$$\lambda_{m,n}^{\text{TM}} = \frac{\pi n_{\text{core}} d}{\gamma_{m,n}}, \quad \lambda_{m,n}^{\text{TE}} = \frac{\pi n_{\text{core}} d}{\psi_{m,n}}$$

A concept of sapphire fiber bundle for THz imaging with sub-wavelength resolution



THZ IMAGING RELYING ON A BUNDLE OF METAL-COATED SAPPHIRE FIBERS:

Optical characterization



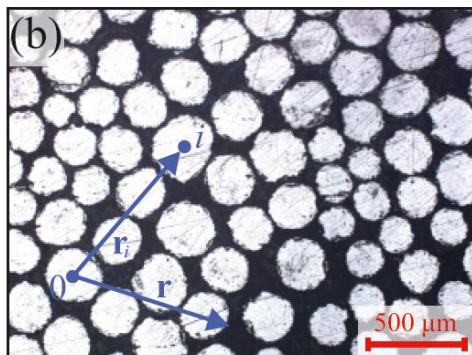
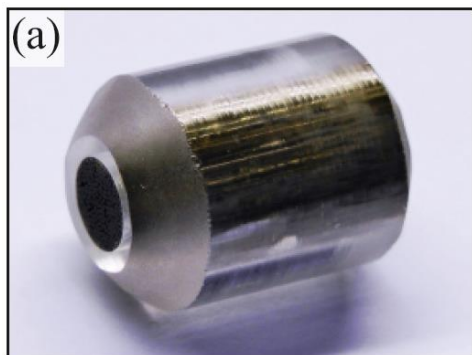
$$n_{\text{eff}} = 1 + \frac{c_0}{2\pi\nu} \frac{1}{(l_2 - l_1)} \phi \left[\frac{F_t^{+1}[E_2]}{F_t^{+1}[E_1]} \right],$$

$$\alpha = \frac{-20}{(l_2 - l_1)} \lg \left| \frac{F_t^{+1}[E_2]}{F_t^{+1}[E_1]} \right|,$$

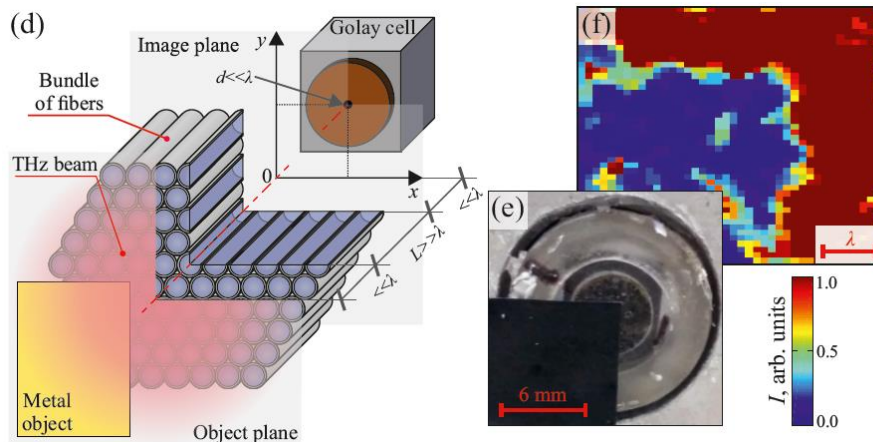
[K.I. Zaytsev et al., *Advanced Optical Materials* (2020), 2020, 2000307]

THZ IMAGING RELYING ON A BUNDLE OF METAL-COATED SAPPHIRE FIBERS

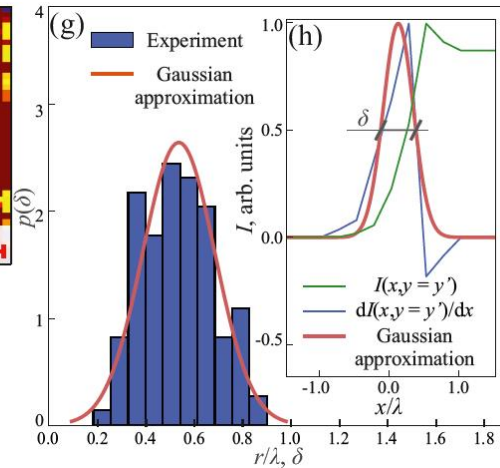
Sample of sapphire bundle



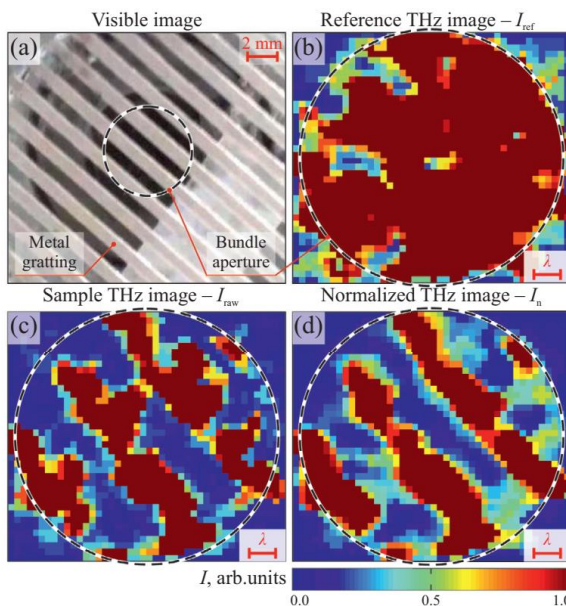
Resolution characterization



$$\langle \delta \rangle = 0.53 \lambda$$



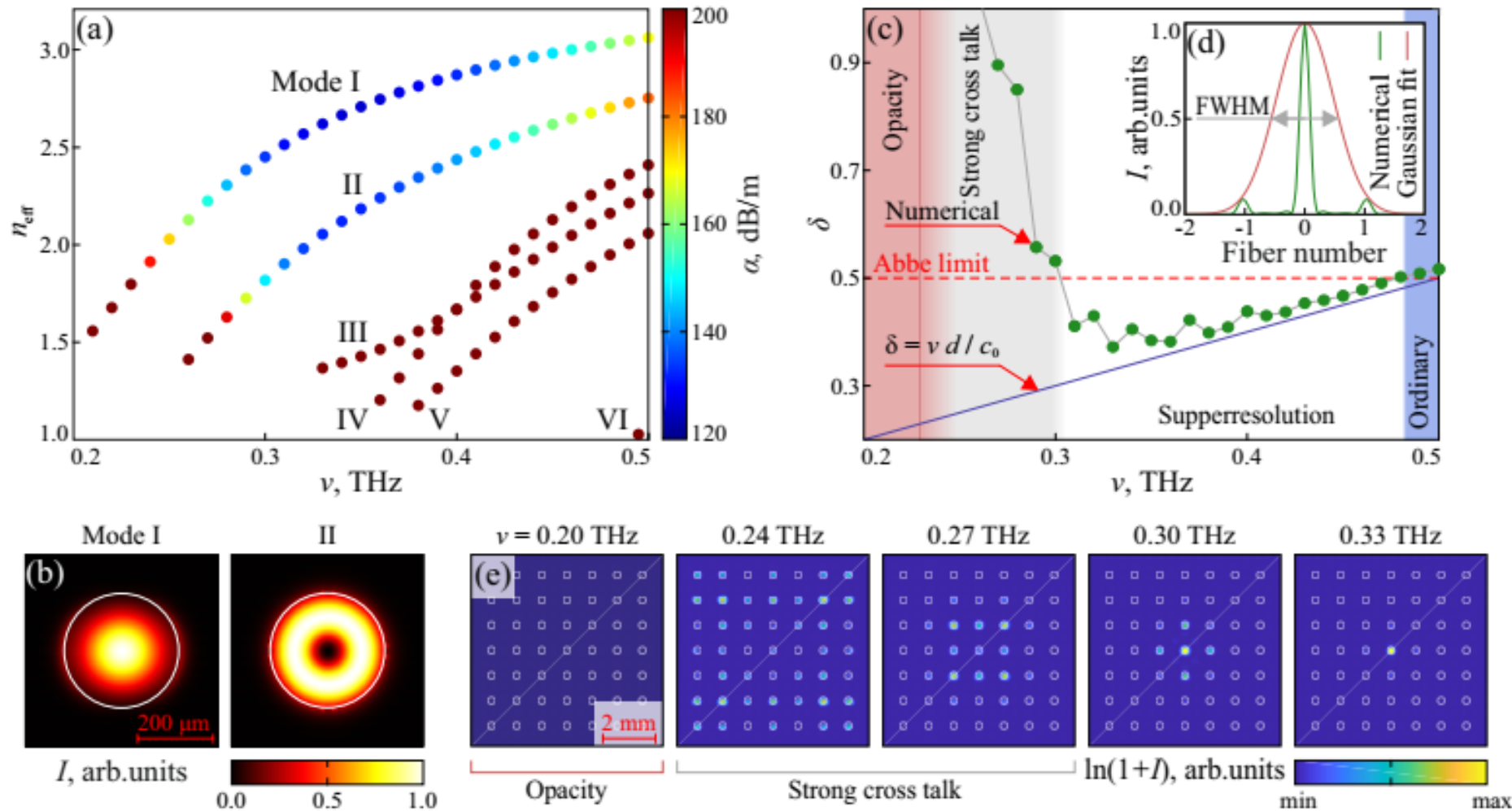
THz imaging of the test object



$$I_n(\mathbf{r}) = \frac{I_{\text{raw}}(\mathbf{r})}{I_{\text{ref}}(\mathbf{r})} \left(1 + \kappa \frac{N}{I_{\text{ref}}(\mathbf{r})} \right)^{-1}$$

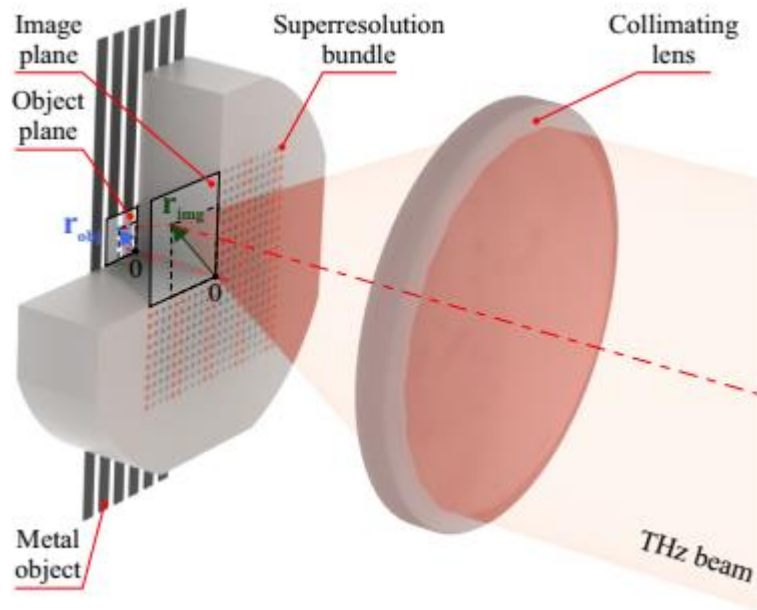
DISADVANTAGES:
energy-inefficient near-field probes (apertures)

TAPERED ALL-DIELECTRIC OPTICAL BUNDLES FOR SUB WAVELENGTH IMAGING WITH USING DIFFRACTION LIMITED OPTICS



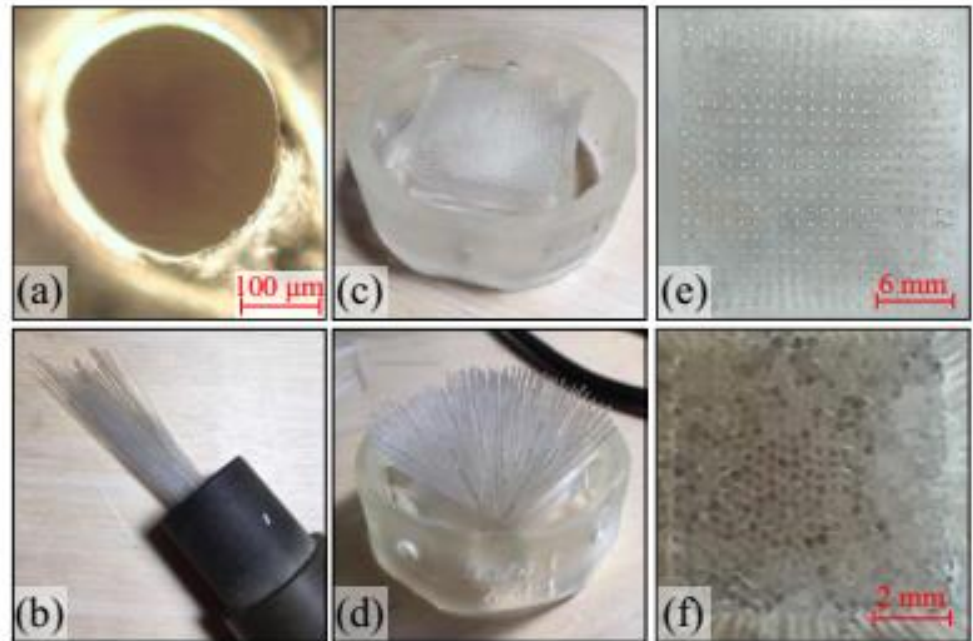
TAPERED ALL-DIELECTRIC OPTICAL BUNDLES FOR SUB WAVELENGTH IMAGING WITH USING DIFFRACTION LIMITED OPTICS

A concept of tapered sapphire fiber bundle for THz imaging with sub-wavelength resolution

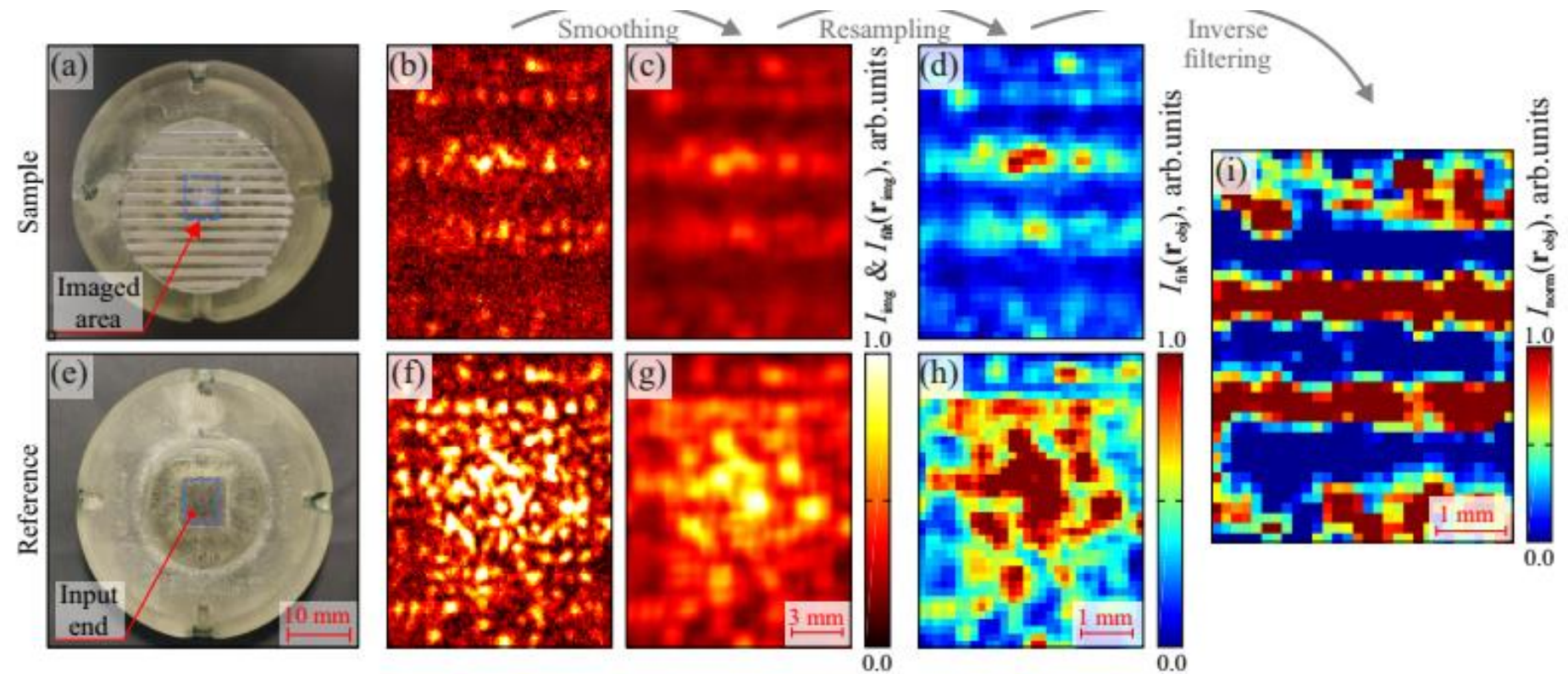


$$\delta = \frac{d}{\lambda} = \frac{d\nu}{c_0}.$$

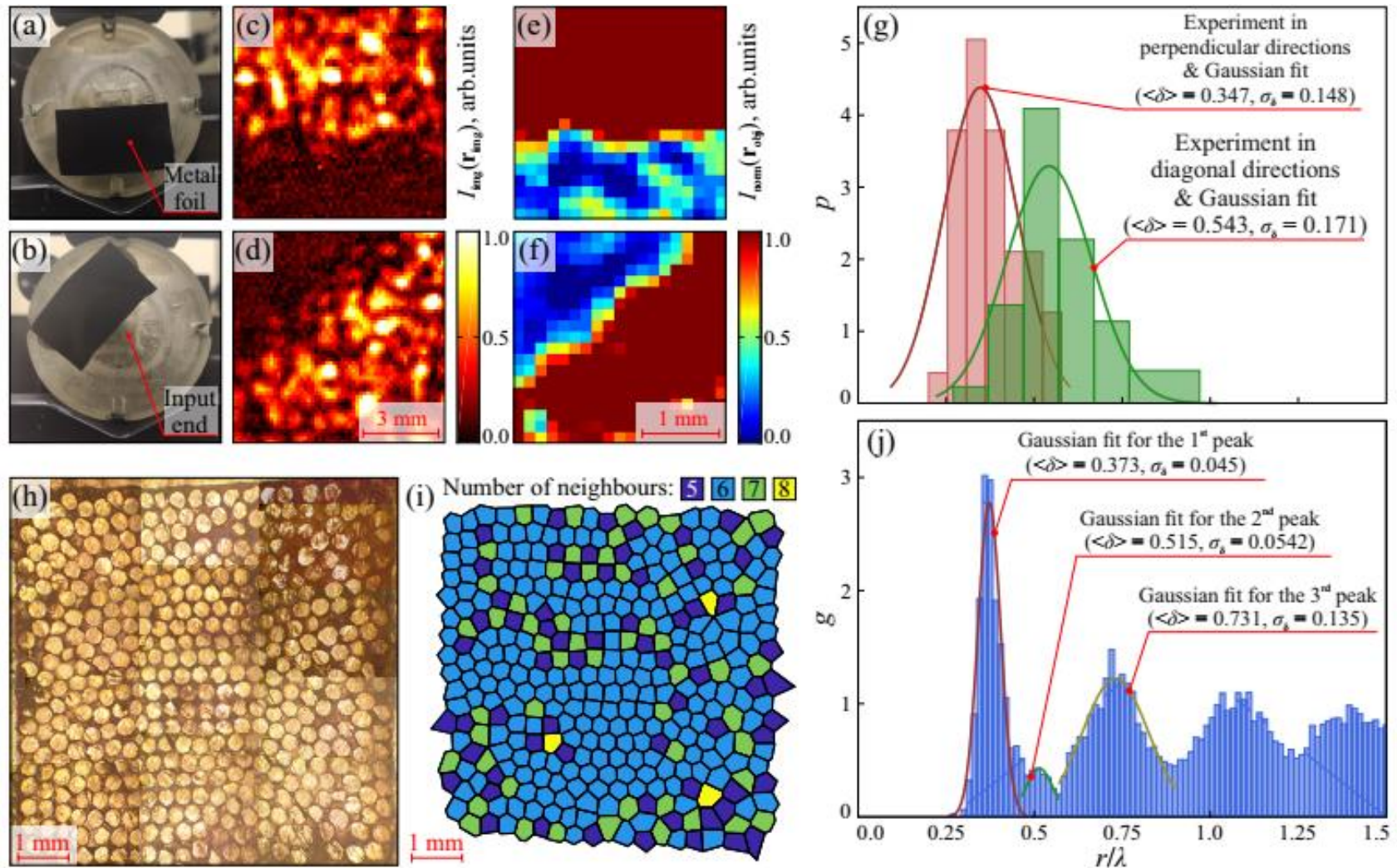
Manufacturing of the sapphire fiber bundle for THz imaging with sub-wavelength resolution



TAPERED ALL-DIELECTRIC OPTICAL BUNDLES FOR SUB WAVELENGTH IMAGING WITH USING DIFFRACTION LIMITED OPTICS



TAPERED ALL-DIELECTRIC OPTICAL BUNDLES FOR SUB WAVELENGTH IMAGING WITH USING DIFFRACTION LIMITED OPTICS



$$\langle \delta \rangle \approx 0.34 \lambda$$

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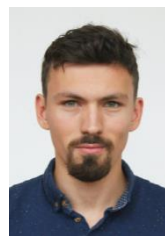
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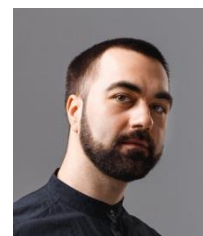
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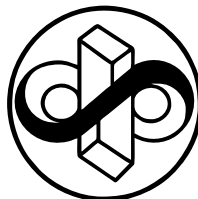
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THANK YOU FOR ATTENTION!